

MEE5114 Advanced Control for Robotics

Lecture 8: Rigid Body Dynamics

Prof. Wei Zhang

CLEAR Lab

Department of Mechanical and Energy Engineering
Southern University of Science and Technology, Shenzhen, China

<https://www.wzhanglab.site/>

Outline

- Spatial Acceleration
- Spatial Force (Wrench)
- Spatial Momentum
- Newton-Euler Equation using Spatial Vectors

Spatial Acceleration

- Given a rigid body with spatial velocity $\mathcal{V} = (\omega, v_o)$, its spatial acceleration is

coordinate free

$$A = \dot{\mathcal{V}} = \begin{bmatrix} \dot{\omega} \\ \dot{v}_o \end{bmatrix} \quad A \triangleq \lim_{\delta \rightarrow 0} \frac{\mathcal{V}(t+\delta) - \mathcal{V}(t)}{\delta}$$

- Recall that: v_o is the velocity of the body-fixed particle coincident with frame origin o at the current time t .

$o \rightarrow$ body-fixed $v_o = \dot{q}$

- Note: $\dot{\omega}$ is the angular acceleration of the body

At time t : $o = q(t)$ $v_o = \dot{q}(t)$, but $\dot{v}_o \neq \ddot{q}(t)$

- \dot{v}_o is not the acceleration of any body-fixed point!

- In fact, \dot{v}_o gives the rate of change in stream velocity of body-fixed particles passing through o



Spatial vs. Conventional Accel. (1/2)

- Why “ \dot{v}_o is not the acceleration of any body-fixed point”?
- Suppose $q(t)$ is the body fixed particle coincides with o at time t_0
- So by definition, we have $v_o(t_0) = \dot{q}(t_0)$, however, $\dot{v}_o(t_0) \neq \ddot{q}(t_0)$, where $\ddot{q}(t_0)$ is the conventional acceleration of the body-fixed point q

- Note: $\dot{v}_o(t_0) \triangleq \lim_{\delta \rightarrow 0} \frac{v_o(t_0 + \delta) - \underbrace{v_o(t_0)}_{\dot{q}(t_0)}}{\delta}$

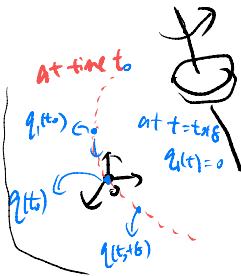
At time $t = t_0$, $q(t_0) = "o" \Rightarrow v_o(t_0) = \dot{q}(t_0)$

At time $t = t_0 + \delta$, $q(t) \neq "o" \Rightarrow v_o(t_0 + \delta) \neq \dot{q}(t_0 + \delta)$

Assume: at $t = t_0 + \delta$, $q_1(t_0 + \delta) = "o" \Rightarrow v_o(t_0 + \delta) = \dot{q}_1(t_0 + \delta)$

Note: q_1 and q were different points:

$$\dot{q}_1(t_0 + \delta) \neq \dot{q}(t_0 + \delta)$$



Spatial vs. Conventional Accel. (2/2) \rightarrow \dot{p} should be $\dot{q}_i(t_0 + \delta)$

$$\Rightarrow \dot{v}_o(t_0) = \lim_{\delta \rightarrow 0} \frac{v_o(t_0 + \delta) - v_o(t_0)}{\delta} \neq \lim_{\delta \rightarrow 0} \frac{\dot{q}(t_0 + \delta) - \dot{q}(t_0)}{\delta} = \ddot{q}(t_0)$$

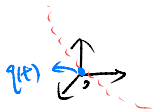
By definition: at all t , we have $\dot{q}(t) = v_o(t) + \omega(t) \times \vec{oq}(t)$
 { we also know (assumed), $q(t_0) = 'o' \Rightarrow \vec{oq}(t_0) = 0$

$$\Rightarrow \boxed{\ddot{q}(t) = \dot{v}_o(t) + \dot{\omega}(t) \times \vec{oq}(t) + \omega(t) \times \dot{q}(t)}$$

$$\text{At } t = t_0; \vec{oq} = 0 \Rightarrow \underline{\underline{\dot{q}(t_0) = \dot{v}_o(t_0) + \omega(t_0) \times \dot{q}(t_0)}}$$

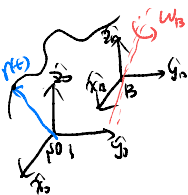
- If $q(t)$ is the body fixed particle coincides with o at time t , then we have

$$\boxed{\ddot{q}(t) = \dot{v}_o(t) + \omega(t) \times \dot{q}(t)} \checkmark$$



Plücker Coordinate System and Basis Vectors (1/3)

- Recall coordinate-free concept: let $r \in \mathbb{R}^3$ be a free vector with $\{o\}$ and $\{B\}$ frame coordinate ${}^o r$ and ${}^B r$



$$r = \begin{bmatrix} r_x \\ r_y \\ r_z \end{bmatrix} \in \mathbb{R}^3 \iff$$

$$r = \begin{bmatrix} \hat{x}_0 & \hat{y}_0 & \hat{z}_0 \end{bmatrix} r \quad \text{--- (1)}$$

$${}^o r = \begin{bmatrix} {}^o r_x \\ {}^o r_y \\ {}^o r_z \end{bmatrix} \in \mathbb{R}^3 \iff$$

$$r = \begin{bmatrix} \hat{x}_B & \hat{y}_B & \hat{z}_B \end{bmatrix} {}^B r \quad \text{--- (2)}$$

express this "physics" in "o" frame

$${}^o r = \underbrace{\begin{bmatrix} {}^o \hat{x}_B & {}^o \hat{y}_B & {}^o \hat{z}_B \end{bmatrix}}_{} {}^B r$$

$$\textcircled{1} \Rightarrow \dot{r} = \begin{bmatrix} \hat{x}_0 & \hat{y}_0 & \hat{z}_0 \end{bmatrix} \frac{d}{dt} ({}^o r)$$

apparent derivative
 $\cong {}^o \dot{r}$

use $\{o\}$ -frame to express physics:

$${}^o (\dot{r}) = \begin{bmatrix} {}^o \hat{x}_0 & {}^o \hat{y}_0 & {}^o \hat{z}_0 \end{bmatrix} \frac{d}{dt} ({}^o r) = \frac{d}{dt} ({}^o r)$$

$$\boxed{{}^o \dot{r} = \frac{d}{dt} ({}^o r)}$$

$\left[\frac{d}{dt} ({}^o r) \right]$ \rightarrow $\frac{d}{dt} ({}^o r)$

Plücker Coordinate System and Basis Vectors (2/3)



② \Rightarrow $r = [\hat{x}_B \ \hat{y}_B \ \hat{z}_B]^B r$...

${}^B(\dot{r}) \neq \underbrace{(\dot{r})'}_{\dot{r}}$ \times if r is changing

$$\dot{\hat{x}}_B = \omega_B \times \hat{x}_B$$

${}^B R_B$

$$\begin{aligned} \dot{r} &= [\dot{\hat{x}}_B \ \dot{\hat{y}}_B \ \dot{\hat{z}}_B]^B r + [\hat{x}_B \ \hat{y}_B \ \hat{z}_B] (\dot{r})' \\ &= \omega_B \times [\hat{x}_B \ \hat{y}_B \ \hat{z}_B]^B r + [\hat{x}_B \ \hat{y}_B \ \hat{z}_B] (\dot{r})' \end{aligned}$$

use $\{B\}$ frame to express "physics"

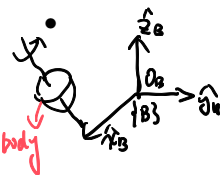
$$\underbrace{{}^B(\dot{r})}_{\downarrow} = \underbrace{{}^B \omega_B \times r}_{\downarrow} + \underbrace{\frac{d}{dt}(r)}_{\downarrow} \triangleq \dot{r}$$

accounts for coordinate frame is moving

due to changes in coordinate

$$\begin{aligned} r &= \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}, & r &= \hat{x}_B \\ & & r &= \hat{y}_B + \hat{z}_B \end{aligned}$$

Plücker Coordinate System and Basis Vectors (3/3)



${}^B V_{\text{body}} = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$, means "body" rotates about \hat{x}_B at unit speed.
 $\Leftrightarrow V_{\text{body}} \triangleq e_{B1}$ ← motion basis vector

$= \begin{bmatrix} 0 \\ 1 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$, means "body" rotates about \hat{y}_B at unit speed.
 $\Leftrightarrow V_{\text{body}} \triangleq e_{B2}$

$= \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ 0 \\ 0 \end{bmatrix}$, means "body" linearly moves along \hat{z}_B at unit speed.
 $\Leftrightarrow V_{\text{body}} \triangleq e_{B3}$

Given $\{B\}$ frame

$\{e_{B1}, e_{B2}, \dots, e_{B6}\}$ -

6 - motion basis vectors

each twist is linear combination of 6 - motion basis vectors

$V_{\text{body}} = \underbrace{v_1 e_{B1} + v_2 e_{B2} + \dots + v_6 e_{B6}}_{\text{coordinate free}}, \text{ where } \begin{bmatrix} v_1 \\ v_2 \\ \vdots \\ v_6 \end{bmatrix} = {}^B V_{\text{body}}$

Work with Moving Reference Frame

• Use $\{b\}$ -frame to express the above physics

$${}^0V_{\text{body}} = \alpha_1 {}^0e_{B_1} + \alpha_2 {}^0e_{B_2} + \dots + \alpha_6 {}^0e_{B_6} = \begin{bmatrix} {}^0e_{B_1} & {}^0e_{B_2} & \dots & {}^0e_{B_6} \end{bmatrix} \Bigg|_{\text{body}}$$

${}^0e_{B_i}$: can be computed from "physics" and twist definition

i : unit speed rotation about \hat{x}_B axis expressed in $\{b\}$

$$\underbrace{\begin{bmatrix} {}^0e_{B_1} & \dots & {}^0e_{B_6} \end{bmatrix}}_{6 \times 6} = {}^0X_B = \text{Ad}_{T_B}$$

$$\left\{ \begin{array}{l} \text{if } {}^0T_B = (R, p) \\ {}^0X_B = \begin{bmatrix} R & 0 \\ \bar{p}R & R \end{bmatrix} \end{array} \right.$$

$$A_{\text{body}} \triangleq \frac{d}{dt} (\mathcal{V}_{\text{body}}) \quad ; \quad \mathcal{V}_{\text{body}} = [e_{B_1} \ e_{B_2} \ \dots \ e_{B_6}]^B \mathcal{V}_{\text{body}}$$

$$\Rightarrow A_{\text{body}} = \underbrace{[\dot{e}_{B_1} \ \dot{e}_{B_2} \ \dots \ \dot{e}_{B_6}]^B}_{\text{express in } \{B\}} \mathcal{V}_{\text{body}} + [e_{B_1} \ \dots \ e_{B_6}]^B \frac{d}{dt} (\mathcal{V}_{\text{body}})$$

① If $\{B\}$ does not change (e.g. $\{0\}$ frame case)

$$\mathcal{V}_{\text{body}} = [e_{B_1} \ \dots \ e_{B_6}]^B \mathcal{V}_{\text{body}}^0 \Rightarrow \mathcal{V}_{\text{body}}^B = \mathcal{V}_{\text{body}}^0$$

$$\triangleq \mathcal{V}_{\text{body}}^B$$

② If $\{B\}$ changes over time, then $\{B\}$ has twist \mathcal{V}_B

$${}^B A_{\text{body}} \neq \mathcal{V}_{\text{body}}^0$$

$$\left(\frac{d}{dt} (\mathcal{V}_{\text{body}}) \right)^B$$

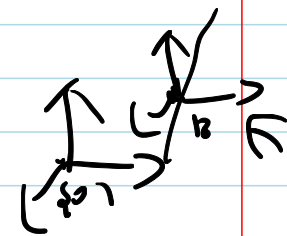
The key is to compute $[\dot{e}_{B_1} \ \dot{e}_{B_2} \ \dots \ \dot{e}_{B_6}]^B \leftarrow$ can be computed purely by physics $= \mathcal{V}_B^B$

Now let's work with "0" frame to find \mathcal{V}_B

(see Featherstone)

$$\Rightarrow \text{we need to compute } [{}^0 \dot{e}_{B_1} \ {}^0 \dot{e}_{B_2} \ \dots \ {}^0 \dot{e}_{B_6}] = \dot{\mathcal{X}}_B = \frac{d}{dt} \left(\text{Ad}_{\mathcal{T}_B} \right)$$

let's denote ${}^0T_B = [R, p] \Rightarrow {}^0\dot{X}_B = \frac{d}{dt} \begin{pmatrix} R & 0 \\ [p]R & R \end{pmatrix}$ $R = [x_B, y_B, z_B]$



0T_B ; $\{B\}$ -frame has instantaneous velocity $v_B = \begin{bmatrix} \omega \\ v_0 \end{bmatrix}$

$$\dot{R} = \omega \times R, \quad ([p]R)' = [\dot{p}]R + [p]\dot{R}$$

Note: $\dot{p} = v_0 + \omega \times p$

$$[\dot{p}] = [v_0 + \omega \times p]$$

$$= [v_0] + [\omega \times p] \leftarrow \text{Jacobi's identity}$$

$$= [v_0] + [\omega][p] - [p][\omega]$$

$$\begin{aligned} &= [v_0]R + [\omega][p]R - \cancel{[p][\omega]R} + \cancel{[p][\omega]R} \\ &= [v_0]R + [\omega][p]R \end{aligned}$$

$$\Rightarrow {}^0\dot{X}_B = \begin{bmatrix} [\omega]R & 0 \\ [v_0]R + [\omega][p]R & [\omega]R \end{bmatrix} = \begin{bmatrix} [\omega] & 0 \\ [v_0] & [\omega] \end{bmatrix} {}^0X_B$$

$$\begin{pmatrix} \dot{X}_B \\ 0 \end{pmatrix} = \underbrace{\begin{bmatrix} [w] & 0 \\ [v_0] & [w] \end{bmatrix}} \begin{matrix} 0 \\ X_B \end{matrix} \equiv \underbrace{\mathcal{V}_B \times}_{\text{6-dim / twist cross /}} X_B$$

spatial cross product.

$$\dot{R}_B = {}^0\omega_B \times {}^0R_B = [{}^0\omega_B] {}^0R_B$$

Notation: Given $\mathcal{V}_i = \begin{bmatrix} w \\ v \end{bmatrix}$, $(\mathcal{V}_i \times) \equiv \begin{bmatrix} [w] & 0 \\ [v] & [w] \end{bmatrix}$

Recall: $[\mathcal{V}] = \begin{bmatrix} [w] & v \\ 0 & 0 \end{bmatrix} \in \text{se}(3)$

In coordinate free: $R_B = [\hat{x}_B \ \hat{y}_B \ \hat{z}_B]$, $\{\mathcal{B}\}$: ω_B rotation

$$\dot{R}_B = \omega_B \times R_B$$

$X_B = [e_{B1} \ e_{B2} \ \dots \ e_{Bn}]$, $\{\mathcal{B}\}$ has twist \mathcal{V}_B

$$\dot{X}_B = \mathcal{V}_B \times X_B$$

$$\dot{e}_{B1} = \mathcal{V}_B \times e_{B1}$$

Derivative of Adjoint

- Suppose a frame $\{A\}$'s pose is $T_A = (R_A, p_A)$, and is moving at an instantaneous velocity $\mathcal{V}_A = (\omega, v)$. Then

$$\underline{\frac{d}{dt}([\text{Ad}_{T_A}] = \begin{bmatrix} [\omega] & 0 \\ [v] & [\omega] \end{bmatrix} [\text{Ad}_{T_A}]}$$

$$\frac{d}{dt}(X_A) = \mathcal{V}_A \times X_A$$

$${}^0 \dot{X}_A = {}^0 \mathcal{V}_A \times {}^0 X_A$$

$${}^A \left(\dot{X}_A \right) = {}^A \mathcal{V}_A \times {}^A X_A$$

Spatial Cross Product

- Given two spatial velocities (twists) \mathcal{V}_1 and \mathcal{V}_2 , their spatial cross product is:

$$\mathcal{V}_1 \times \mathcal{V}_2 = \begin{bmatrix} \omega_1 \\ v_1 \end{bmatrix} \times \begin{bmatrix} \omega_2 \\ v_2 \end{bmatrix} \triangleq \begin{bmatrix} \omega_1 \times \omega_2 \\ \omega_1 \times v_2 + v_1 \times \omega_2 \end{bmatrix}$$

Lie Bracket

- Matrix representation: $\mathcal{V}_1 \times \mathcal{V}_2 = [\mathcal{V}_1 \times] \mathcal{V}_2$, where

$$[\mathcal{V}_1 \times] \triangleq \begin{bmatrix} [\omega_1] & 0 \\ [v_1] & [\omega_1] \end{bmatrix}$$

- Roughly speaking, when a motion vector \mathcal{V} is moving with a spatial velocity \mathcal{Z} (e.g. it is attached to a moving frame) but is otherwise not changing, then

$$\dot{\mathcal{V}} = \mathcal{Z} \times \mathcal{V}$$

Spatial Cross Product: Properties (1/1)

- Assume A is moving wrt to O with velocity \mathcal{V}_A

$${}^o\dot{X}_A = [{}^o\mathcal{V}_A \times] {}^oX_A$$

- $[X\mathcal{V}\times] = X[\mathcal{V}\times]X^T$, for any transformation X and twist \mathcal{V}



$$[R\omega] = R[\omega]R^T$$

Spatial Acceleration with Moving Reference Frame

Consider a body with velocity \mathcal{V}_{body} (wrt inertia frame), and ${}^O\mathcal{V}_{body}$ and ${}^B\mathcal{V}_{body}$ be its Plücker coordinates wrt $\{O\}$ and $\{B\}$:

$$\bullet \quad {}^B A_{body} = \frac{d}{dt} ({}^B \mathcal{V}_{body}) + \underbrace{{}^B \mathcal{V}_B \times {}^B \mathcal{V}_{body}}_{\text{apparent derivative}} \leftarrow \text{due to frame } \{B\} \text{ is moving}$$

$${}^B \left(\frac{d}{dt} (\mathcal{V}_{body}) \right)$$

$${}^B \dot{\mathcal{V}}_{body}$$

\mathcal{V}_B : frame $\{B\}$ twist

\mathcal{V}_{body} : body velocity twist

$$\bullet \quad {}^O A = {}^O X_B {}^B A \rightarrow {}^B \left(\frac{d}{dt} (\mathcal{V}_{body}) \right)$$

$${}^O \left(\frac{d}{dt} (\mathcal{V}_{body}) \right)$$

$\{B\}$ frame does not change

$${}^O (A_{body}) = \frac{d}{dt} ({}^O \mathcal{V}_{body}) = \frac{d}{dt} ({}^O X_B {}^B \mathcal{V}_{body}) = \underbrace{{}^O \dot{X}_B} {}^B \mathcal{V}_{body} + {}^O X_B \dot{{}^B \mathcal{V}_{body}}$$

$$= [{}^O \mathcal{V}_B \times] {}^O X_B {}^B \mathcal{V}_{body} + ({}^O X_B) \dot{{}^B \mathcal{V}_{body}}$$

$$= {}^O X_B \left\{ \underbrace{{}^B X_O [{}^O \mathcal{V}_B \times] {}^O X_B} {}^B \mathcal{V}_{body} + \dot{{}^B \mathcal{V}_{body}} \right\} \dots \otimes$$

Spatial Acceleration Example

Find ${}^B A_{top} = {}^B \left(\frac{d}{dt} V_{top} \right)$

Method 1:

$$= {}^B \dot{V}_{top} + {}^B \omega_B \times {}^B V_{top}$$

$${}^B V_{top} = \begin{bmatrix} 0 \\ 0 \\ 50 \\ \vdots \\ -0.2 \\ 0 \end{bmatrix} \quad {}^B \omega = \begin{bmatrix} 0 \\ 0 \\ 50 \text{ rad/s} \end{bmatrix}$$

$${}^B \omega_B = \begin{bmatrix} 0 \\ 0.02 \\ 0 \end{bmatrix}$$

$${}^B A_{top} = \frac{d}{dt} ({}^B V_{top}) + {}^B V_{Bframe} \times {}^B V_{top}$$

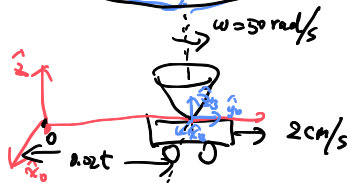
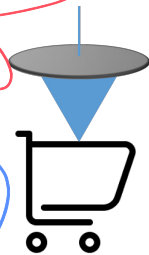
$$= \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0.02 \\ 0 \end{bmatrix} \times \begin{bmatrix} 0 \\ 0 \\ 50 \\ \vdots \\ -0.2 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

$$\left[{}^B \omega_B \times {}^B V_{top} \right] = \left[{}^B V_{Bframe} \right]$$

$$\Rightarrow \otimes = \omega_B \left\{ {}^B V_{top} \times {}^B V_{body} + {}^B V_{body} \right\}$$

$${}^B \left(\frac{d}{dt} (V_{body}) \right)$$

${}^B V_{body}$



$$\begin{bmatrix} [\omega] \\ [v] \end{bmatrix} \begin{bmatrix} 0 \\ \omega \end{bmatrix}$$

Outline Method 2: use dof frame

$$\dot{A} = \frac{d}{dt} ({}^0V_{top})$$

$${}^0V_{top} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$$

$$v_6 = \begin{bmatrix} 50 \text{ km/h} \\ 0.02 \\ 0 \end{bmatrix}$$

- Spatial Acceleration

$${}^0A = \begin{bmatrix} 0 \\ 0 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$$

- Spatial Force (Wrench)

$${}^B A = {}^B X_0 \cdot {}^0 A$$

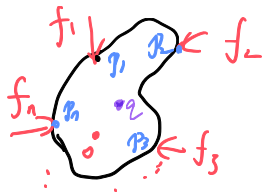
- Spatial Momentum

$$= \begin{bmatrix} I & 0 \\ 0 & I \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ 0 \\ \vdots \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$$

- Newton-Euler Equation using Spatial Vectors

Spatial Force (Wrench)

- Consider a rigid body with many forces on it and fix an arbitrary point O in space



- The net effect of these forces can be expressed as
 - A force f , acting along a line passing through O

$$f = \sum_i f_i$$

- A moment n_O about point O

$$n_O = \sum_i (\overrightarrow{Op_i}) \times f_i$$

- Spatial Force (Wrench):** is given by the 6D vector

$$F = \begin{bmatrix} n_O \\ f \end{bmatrix} \leftarrow \text{wrench}$$

recall:

$$V_q = V_O + \omega \times \overrightarrow{Oq}$$

what if we change reference point from "o" to "q"

$$\begin{aligned} n_q &= \sum_i (\overrightarrow{qP_i}) \times f_i = n_O + \sum_i (\overrightarrow{qP_i} \times f_i - \overrightarrow{Op_i} \times f_i) \\ &\text{by definition} \qquad \qquad \qquad = n_O + \sum_i (\overrightarrow{qP_i} - \overrightarrow{Op_i}) \times f_i \end{aligned}$$

Spatial Force in Plücker Coordinate Systems

$$= n_0 + \sum_i q_i \vec{p}_i \times \vec{f}_i$$

$$= n_0 + \vec{q} \times \vec{f}$$

$$= \underline{n_0 + \vec{f} \times \vec{oq}}$$

Given a frame {A}, the Plücker coordinate of a spatial force \mathcal{F} is given by
 convention: choose frame origin as reference point.

$${}^A\mathcal{F} = \begin{bmatrix} {}^A n_{oA} \\ {}^A \vec{f} \end{bmatrix}$$

Coordinate transform: ${}^A\mathcal{F} = {}^A X_B^* {}^B\mathcal{F}$ where ${}^A X_B^* = {}^B X_A^T$

$$\vec{nq} = n_0 + \vec{f} \times \vec{oq}$$

$$= n_0 + \vec{q} \times \vec{f}$$

Frame {A}, {B}, with ${}^A T_B = ({}^A R_B, {}^A p_B)$

$${}^A \mathcal{F} = \begin{bmatrix} {}^A n_{oA} \\ {}^A \vec{f} \end{bmatrix}, \quad {}^B \mathcal{F} = \begin{bmatrix} {}^B n_{oB} \\ {}^B \vec{f} \end{bmatrix}$$



• ${}^A \vec{f} = {}^A R_B {}^B \vec{f} \dots \textcircled{1}$

• moment: coordinate-free:

$$\underline{n_{oA} = n_{oB} + (\vec{f} \times ({}^B \vec{o}_A))}$$

choose {A} frame to express:

$${}^A n_{oA} = {}^A R_B {}^B n_{oB} + {}^A R_B ({}^B \vec{f} \times ({}^B \vec{o}_A))$$

$$= {}^A R_B ({}^B n_{oB} + (-{}^B p_A) \times {}^B \vec{f}) \dots \textcircled{2}$$

$$\begin{matrix} ① \\ ② \end{matrix} \Rightarrow \begin{bmatrix} {}^A n_A \\ \underline{{}^A f} \end{bmatrix} = \underbrace{\begin{bmatrix} {}^A R_B & \vdots & -{}^A R_B [{}^B p_A] \\ 0 & \vdots & {}^A R_B \end{bmatrix}}_{\triangleq \underline{{}^A X_B}^*} \begin{bmatrix} {}^B n_B \\ \underline{{}^B f} \end{bmatrix}$$

$$[a]^T = -[a]$$

$${}^B X_A = \begin{bmatrix} {}^B R_A & \vdots & 0 \\ \vdots & \vdots & \vdots \\ [{}^B p_A] {}^B R_A & \vdots & {}^B R_A \end{bmatrix}, \quad {}^B X_A^T = \begin{bmatrix} {}^A R_B & \vdots & -{}^A R_B [{}^B p_A] \\ \vdots & \vdots & \vdots \\ 0 & \vdots & {}^A R_B \end{bmatrix}$$

$$\Rightarrow \underline{{}^A X_B}^* = \left({}^B X_A \right)^T$$

Wrench-Twist Pair and Power



$$P_{\text{power}} = f^T v = \langle f, v \rangle$$

- Recall that for a point mass with linear velocity v and linear force f . Then we know that the power (instantaneous work done by f) is given by $f \cdot v = f^T v$
- This relation can be generalized to spatial force (i.e. wrench) and spatial velocity (i.e. twist)
- Suppose a rigid body has a twist $\mathcal{V} = ({}^A\omega, {}^A v_{O_A})$ and a wrench $\mathcal{F} = ({}^A n_{O_A}, {}^A f)$ acts on the body. Then the power is simply

$$\underbrace{P}_{\text{Scalar}} = \underbrace{({}^A\mathcal{V})^T}_{(1 \times 6)} \underbrace{{}^A\mathcal{F}}_{(6 \times 1)} = \mathcal{F}^T \mathcal{V}$$

$$= \underbrace{({}^A\omega)^T ({}^A n_{O_A})}_{\text{rotational power}} + \underbrace{{}^A v_{O_A}^T {}^A f}$$

Joint Torque

- Consider a link attached to a 1-dof joint (e.g. revolute or prismatic). Let \hat{S} be the screw axis of the joint. The velocity of the link induced by joint motion is given by: $\mathcal{V} = \hat{S}\dot{\theta}$



- \mathcal{F} be the wrench provided by the joint. Then the power produced by the joint is

$$P = \mathcal{V}^T \mathcal{F} = (\hat{S}^T \mathcal{F}) \dot{\theta} \triangleq \tau \dot{\theta}$$

$\hat{S} \dot{\theta}$ $\tau \triangleq \hat{S}^T \mathcal{F} = \mathcal{F}^T \hat{S}$
 6×1 6×1

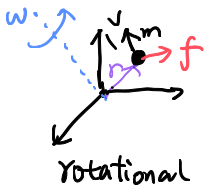
- $\tau = \hat{S}^T \mathcal{F} = \mathcal{F}^T \hat{S}$ is the projection of the wrench onto the screw axis, i.e. the effective part of the wrench.
- Often times, τ is referred to as joint "torque" or generalized force

Outline

- Spatial Acceleration
- Spatial Force (Wrench)
- **Spatial Momentum**
- Newton-Euler Equation using Spatial Vectors

Rotational Inertia (1/2)

- Recall momentum for point mass:



Linear motion:

velocity: $v = \dot{r}$, $a = \dot{v} = \ddot{r} \in \mathbb{R}^3 \leftrightarrow$

force: $f = ma = m\dot{v} = m\ddot{r}$

Linear momentum: $L = m \cdot v$

$\underline{\omega} = \hat{\omega} \hat{\theta}$, $v = \underline{\omega} \times r$

\leftrightarrow moment: $n = r \times f$

\leftrightarrow Angular momentum:

$\phi = r \times L$

$= r \times (m \underline{\omega} \times r)$

$= m [r] [-r] \underline{\omega}$

$\phi = \bar{I} \omega$

Scalar \downarrow 3×3 \downarrow 3×3 \rightarrow Inertia matrix

$m [r] [r]^T$

Rotational Inertia (2/2)

- Rotational Inertia: $\bar{I} = \int_V \rho(r) [r][r]^T dr$ \rightarrow print mass 做积**分**.

- $\rho(\cdot)$ is the density function of the body

- \bar{I} depends on coordinate system

- It is a constant matrix if the origin coincides with CoM

What's def of Center of Mass:

$$C \triangleq \text{CoM} = \frac{1}{m} \int \rho(r) r \, dV$$

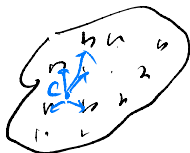
$$\circ \quad C \approx \frac{1}{m} \sum m_i r_i$$

If C is CoM, then $\frac{1}{m} \sum m_i (C r_i) = 0$

$$\Rightarrow \sum m_i C r_i = 0 \Rightarrow \sum m_i [C r_i] = 0 \dots \textcircled{1}$$

$$\phi = \left(\sum_i m_i [L r_i] [L r_i]^T \right) \omega$$

this matrix depends on coordinate system



Spatial Momentum

- Consider a rigid body with spatial velocity $v_C = (\omega, v_C)$ expressed at the center of mass C (derivation below works only when $c = C.M.$)

- Linear momentum:

$L \triangleq m v_C$ velocity of CoM (why?) \rightarrow g-int mass m 's velocity

- Angular momentum about CoM:

$\phi_c \triangleq \bar{I}_c \omega$ $\leftarrow \phi_c = \sum_i \overrightarrow{cr_i} \times (m_i v_i) = \sum_i \overrightarrow{cr_i} \times$

- Angular momentum about a point O :

$\phi_o = \sum_i \overrightarrow{or_i} \times (m_i v_i) \stackrel{\text{by definition}}{=} \phi_c + \overrightarrow{oc} \times L$ $\stackrel{\text{v.f.y.}}{=} (m v_c + m_i \omega \times \overrightarrow{cr_i})$

$= \sum_i (m_i v_c + m_i \omega \times \overrightarrow{cr_i}) = m v_c + \underbrace{\left(\sum_i m_i \overrightarrow{cr_i} \right)}_{=0} \times \omega$

• Spatial Momentum:

$h \triangleq \begin{bmatrix} \phi \\ L \end{bmatrix}$ reference point \downarrow convention: chosen to be origin of coordinate system.

$\phi_o = \phi_c + \overrightarrow{oc} \times L$ \leftarrow coordinate free

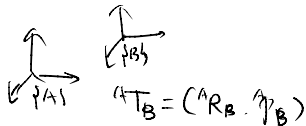
$h = m v_c$ \leftarrow $h_c = \bar{I}_c \omega$

mass: m
rotational inertia: \bar{I}_c

Change Reference Frame for Momentum

$$\begin{aligned} \vec{v}_q &= \vec{v}_c + \omega \times \vec{r}_q \\ \dot{r}_q &= \dot{r}_c + \dot{q} \vec{e} \times \vec{r}_q \end{aligned}$$

- Spatial momentum transforms in the same way as spatial forces:



$$\underline{{}^A h = {}^A X_B^* {}^B h}$$

$${}^B h = \begin{bmatrix} {}^B \phi_{0B} \\ {}^B L \end{bmatrix}$$

${}^A \phi_{0B}$ is a valid notion

$${}^A L = {}^A R_B {}^B L$$

$${}^A h = \begin{bmatrix} {}^A \phi_{0A} \\ {}^A L \end{bmatrix}$$

$$\underbrace{\phi_{0A} = \phi_{0B} + ({}^A \sigma_B \times L)}_{\text{coordinate-free } (2)}$$

$$\Rightarrow {}^A h = ({}^A X_B^*) {}^B h$$

same as change of coordinate for wrench

Spatial Inertia

h : similar to force F : think about inertia matrix as mapping from motion space M to Force space F

- Inertia of a rigid body defines linear relationship between velocity and momentum.

- Spatial inertia \mathcal{I} is the one such that

$$h = \mathcal{I}V$$

- Let $\{C\}$ be a frame whose origin coincide with CoM. Then

Force space: F

twist V

Acceleration A

wrench

Momentum

motion space

$$\underbrace{{}^c\mathcal{I}}_{\substack{b \times b \\ \text{matrix}}} = \begin{bmatrix} \frac{{}^c\bar{I}_c}{0} & 0 \\ 0 & m\underbrace{I_3}_{\substack{3 \times 3 \text{ identity matrix}}} \end{bmatrix}$$

In this case, we know

$${}^c\gamma = \begin{bmatrix} {}^c\omega \\ {}^cV_c \end{bmatrix}, \quad {}^cV_{com} = {}^cV_c \Rightarrow {}^cL = m {}^cV_c$$

$${}^c\phi_c = {}^c\bar{I}_c {}^c\omega$$

$${}^c h = \begin{bmatrix} {}^c\bar{I}_c {}^c\omega \\ m {}^cV_c \end{bmatrix} = \underbrace{\begin{bmatrix} {}^c\bar{I}_c & 0 \\ 0 & mI_{3 \times 3} \end{bmatrix}}_{\text{Spatial Inertia Matrix}} \begin{bmatrix} {}^c\omega \\ {}^cV_c \end{bmatrix}$$

Spatial Inertia

$$\mathbb{R}_B \mathbb{R}_O + \mathbb{R}_C$$

- Spatial inertia wrt another frame $\{A\}$:

$$\boxed{{}^A I = {}^A X_C^* {}^C I {}^C X_A}$$

$$\underbrace{{}^A h = ({}^A p) A v}_{\text{frame } A} = \underbrace{{}^A X_C^* c h}_{\text{frame } C} = {}^A X_C^* {}^C I {}^C v = ({}^A X_C^* {}^C I {}^C X_A) A v$$

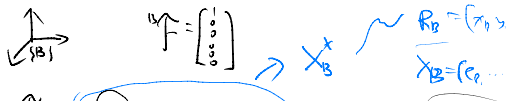
- Special case: $\underline{{}^A R_C = I_3}$ (A 's orientation is the same as $\{C\}$)

we know: ${}^A X_C = \begin{bmatrix} I_2 & 0 \\ [{}^A p_C] & I_2 \end{bmatrix}$

$${}^A I = \begin{bmatrix} {}^C I + m [{}^A p_C] [{}^A p_C]^T & m [{}^A p_C] \\ m [{}^A p_C] & m I_{1,3} \end{bmatrix} \quad \text{X}$$



Outline



- Spatial Acceleration

- Spatial Force (Wrench)



- Spatial Momentum

$$A_{R_0} = I$$

It turns out (if $\{B\}$ has velocity v_B)

- Newton-Euler Equation using Spatial Vectors

$$\dot{X}_B^* = v_B^* X_B^*$$

where " x^* " defined as:

$$V = \begin{bmatrix} w \\ v \end{bmatrix}, \quad F = \begin{bmatrix} n \\ f \end{bmatrix}, \quad V X^* F \triangleq \begin{bmatrix} w \times n + v \times f \\ w \times f \end{bmatrix} =$$

\rightarrow basis vectors for wrench
 \rightarrow coordinate-free expression

$$\dot{F} = \dot{X}_B^* F + X_B^* (\dot{F})$$

\rightarrow \dot{F} de

Cross Product for Spatial Force and Momentum

Assume frame A is moving with velocity ${}^A V_A$

$$\bullet \quad {}^A \left[\frac{d}{dt} \mathcal{F} \right] = \underbrace{\frac{d}{dt} ({}^A \mathcal{F})}_{\text{coordinate free}} + \underbrace{{}^A \mathcal{V} \times {}^A \mathcal{F}}_{\text{apparent derivative}}$$

Recall: ${}^A \left(\frac{d}{dt} v_{body} \right) = \frac{d}{dt} ({}^A v_{body}) + {}^A \mathcal{V}_A \times {}^A v_{body}$

$$\bullet \quad {}^A \left[\frac{d}{dt} h \right] = \frac{d}{dt} ({}^A h) + {}^A \mathcal{V} \times {}^A h$$

or equivalently

$$[{}^A \mathcal{V} \times {}^A \mathcal{F}] = \begin{bmatrix} [\omega] & [v] \\ 0 & [\omega] \end{bmatrix}$$

$$\dot{X}_B^* = [{}^A \mathcal{V}_A \times X^*] X_B^k$$

you can choose "i" frame to derive this

Fact: $[{}^A \mathcal{V} \times {}^A \mathcal{F}] = -[{}^A \mathcal{V} \times {}^A \mathcal{F}]^T$

$$\dot{\mathcal{F}} = X_B^* \dot{\mathcal{F}} + [{}^A \mathcal{V}_A \times X^*] X_B^* \mathcal{F}$$

use X_B^* to express this physics

$${}^A \dot{\mathcal{F}} = B \dot{\mathcal{F}} + [{}^A \mathcal{V}_A \times X^*] B \mathcal{F}$$

\dot{v}

Newton-Euler Equation

- Newton-Euler equation:



net wrench
applied to
the body

coordinate-free

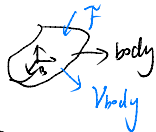
i.e. its form
does not depend on
coordinate-system

$$F = \frac{d}{dt}h = \underline{IA + V \times^* IV}$$

- Adopting spatial vectors, the Newton-Euler equation has the same form in any frame

$$F \equiv \frac{d}{dt}(h) = \frac{d}{dt}(IV) = IV + \dot{I}V$$

Let's work with inertia frame $\{1\}$ to
derive the NE-equation:



Assumptions:

- dBS: body fixed

$\Rightarrow V_B = \underline{V_{body}}$, ${}^B I$ constant.

$$= \underline{IA} + \dot{I}V$$

due to V (velocity)
is changing

due to inertia
is changing

Derivations of Newton-Euler Equation

$$\bullet \quad \overset{\circ}{f} = \overset{\circ}{\left(\frac{d}{dt}h\right)} = \frac{d}{dt}(\overset{\circ}{h}) = \frac{d}{dt}(\overset{\circ}{I}\overset{\circ}{v}) = \overset{\circ}{\dot{I}}\overset{\circ}{v} + \overset{\circ}{I}\overset{\circ}{\dot{A}}$$

$$= \frac{d}{dt}(\overset{\circ}{X}_B^* \overset{B}{I} \overset{B}{X}_0) \overset{\circ}{v} + \overset{\circ}{I}\overset{\circ}{\dot{A}}$$

$$= \underbrace{\overset{\circ}{\dot{X}}_B^* \overset{B}{I} \overset{B}{X}_0} \overset{\circ}{v} + \underbrace{\overset{\circ}{X}_B^* \overset{B}{I} \overset{B}{\dot{X}}_0} \overset{\circ}{v} + \overset{\circ}{I}\overset{\circ}{\dot{A}}$$

$$= [\overset{B}{v}_B^*] \underbrace{(\overset{\circ}{X}_B^* \overset{B}{I} \overset{B}{X}_0)} \overset{\circ}{v}$$

$$- \overset{\circ}{X}_B^* \overset{B}{I} \overset{B}{X}_0 [\overset{\circ}{v}_B^*] \overset{\circ}{v} + \overset{\circ}{I}\overset{\circ}{\dot{A}}$$

$\overset{\circ}{v} = \overset{\circ}{v}_B$

$$= [\overset{B}{v}_B^*] \overset{\circ}{I}\overset{\circ}{v} - 0 + \overset{\circ}{I}\overset{\circ}{\dot{A}}$$

$$= \overset{\circ}{I}\overset{\circ}{\dot{A}} + \underbrace{(\overset{\circ}{v}_B^*)^* \overset{B}{I} \overset{B}{X}_0} \overset{\circ}{v}$$

choose any frame: ${}^B f = {}^B I \overset{\circ}{\dot{A}} + {}^B v^* \overset{B}{I} \overset{B}{X}_0$

side note

${}^B \dot{X}_0$?

- we know

$$\overset{\circ}{X}_B = [{}^B v_B^*] \overset{B}{X}_B$$

$$(\overset{\circ}{X}_B^* \overset{B}{X}_0)^{\circ} = I$$

$$\overset{\circ}{X}_B^* \overset{B}{X}_0 + \overset{\circ}{X}_B^* \overset{B}{\dot{X}}_0 = 0$$

$$\overset{B}{\dot{X}}_0 = - \overset{B}{X}_0^{\circ} \overset{\circ}{X}_B^* \overset{B}{X}_0$$

$$= - \overset{B}{X}_0 [{}^B v_B^*] \overset{\circ}{X}_B^* \overset{B}{X}_0$$

$$= - \overset{B}{X}_0 [{}^B v_B^*]$$

More Discussions

- Review/summary:

$\begin{bmatrix} \dot{w} \\ \dot{v}_0 \end{bmatrix}$ coordinate-free.

- spatial acceleration: $A \in \mathbb{R}^6$. $A_{body} \triangleq \lim_{\delta \rightarrow 0} \frac{V_{body}(t+\delta) - V_{body}(t)}{\delta}$

- working with inertia/stationary frame: $\triangleq \dot{V}_{body}$

$${}^0 \left(\frac{d}{dt} V_{body} \right) \leftarrow {}^0 A_{body} = \frac{d}{dt} ({}^0 V_{body})$$

- working with moving frame: (suppress $\{B\}$ is moving) $\underbrace{\text{apparent derivative}}_{} \dot{V}_{body}$

$${}^B A_{body} \neq ({}^B V_{body})'$$

spatial cross product

$${}^B A_{body} = \frac{d}{dt} ({}^B V_{body}) + ({}^B V_B \times) {}^B V_{body}$$

$$V_x \triangleq \underbrace{[V_x]}_{6 \times 6} = \begin{bmatrix} [w]_0 \\ [v]_0 \end{bmatrix}$$

$${}^0 A_{body} = {}^B X_0 ({}^B A_{body})$$

$$[v]_{4 \times 4} = \begin{bmatrix} [w]_0 & v \\ 0 & 0 \end{bmatrix}$$

JAS

- Recall: $\dot{R}_A = \omega_A \times R_A$, $[R\omega] = R[\omega]R^T$

Corresponding: ${}^0\dot{X}_A = \underbrace{{}^0V_A}_{6 \times 1} \times {}^0X_A$, $\underbrace{[XVx]}_{6 \times 1} = \underline{X[Vx]X^T}$

More Discussions

- Review / Summary.

- spatial acceleration: $A \in \mathbb{R}^3$ $A_{body} \triangleq \lim_{\delta \rightarrow 0} \frac{V_{body}(t+\delta) - V_{body}(t)}{\delta} \triangleq \dot{V}_{body}$. ↑ coordinate free.

- working with inertia / stationary frame:

$${}^0 \left(\frac{d}{dt} V_{body} \right) \triangleq {}^0 A_{body} = \frac{d}{dt} ({}^0 V_{body})$$

apparent derivative ${}^0 \dot{V}_{body}$

- working with moving frame: (suppose $\{B\}$ is moving).

$${}^B A_{body} \neq ({}^B \dot{V}_{body})'$$

$${}^B A_{body} = \frac{d}{dt} ({}^B V_{body}) + \boxed{{}^B V_B \times} {}^B V_{body}$$

spatial cross product.

$${}^B A_{body} = {}^B X_0 ({}^0 A_{body})$$

screw axis

$${}_{4 \times 4} [v] = \begin{bmatrix} [w] & v \\ 0 & 0 \end{bmatrix}$$

$${}_{b \times b} V_x \triangleq [V_x] = \begin{bmatrix} [w] & 0 \\ [v] & [w] \end{bmatrix}$$

More Discussions

- Recall: $\dot{R}_A = W_A \times R_A$. $|RW| = R|W|R^T$
 \downarrow
 coordinate free.

corresponding: ${}^0\dot{X}_A = \underbrace{{}^0V_A \times^0}_{\text{spatial cross product.}}$ X_A . $[XVx] = X[Vx]X^T$.

spatial force/wrench: ${}^B\mathcal{F} = \begin{bmatrix} {}^B N_B \\ {}^B f \end{bmatrix}$ ${}^A\mathcal{F} = {}^A X_B^* {}^B\mathcal{F}$

$$\begin{aligned} {}^0\dot{X}_A^* &= V_A X^* {}^0\dot{X}_A^* \\ &= \underbrace{[V_A X^*]}_{6 \times 6} {}^0\dot{X}_A^* \end{aligned}$$

$${}^A X_B^* = ({}^B X_A)^T$$

Joint torque.

$$\tau \dot{\theta} = v^T \mathcal{F} = (s^T \dot{\theta}) \mathcal{F}$$

$$\tau = s^T \mathcal{F} = \mathcal{F}^T s$$

More Discussions

spatial momentum:

$${}^A h = \begin{bmatrix} {}^A \phi_A \\ {}^A L \end{bmatrix}, \quad {}^A h = {}^A X_B^* {}^B h$$

• spatial inertia matrix \mathcal{I} (COM frame)

$${}^C \mathcal{I} = \begin{bmatrix} {}^C \mathcal{I} & \vdots & 0 \\ \vdots & \ddots & \vdots \\ \cdot & \cdot & (m I_3) \end{bmatrix}$$

$${}^A \mathcal{I} = {}^A X_C^* {}^C \mathcal{I} {}^C X_A$$

NE:

$$\dot{h} = \frac{d}{dt}(h) = \mathcal{I}A + V \times^b \mathcal{I}V$$